

**Gas Turbines: Sub 2 ppm  
NOx Compliance  
Challenges...CARB  
Update**



**CEMTEK User Group  
Meeting  
Costa Mesa, CA**

**Presented by Ben Sehgal  
California Air Resources Board  
September 2016**

# Objectives

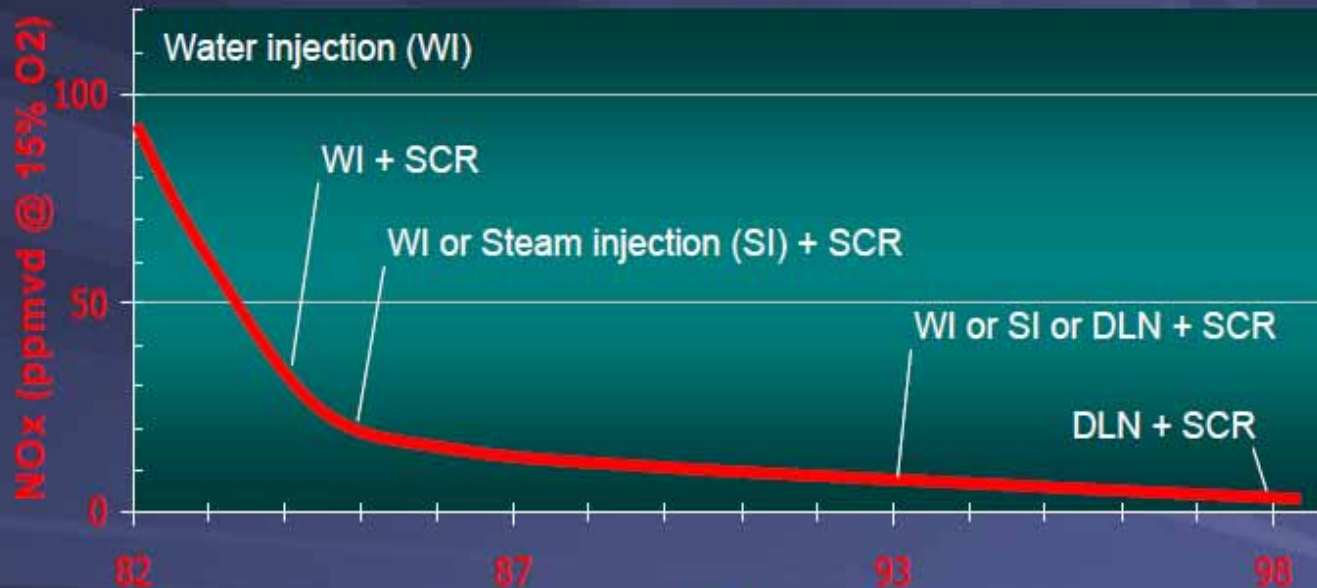
- x **Comprehend gas turbine technological feasibility of sub 2ppm NO<sub>x</sub> Levels regulations and its national impact on BACT**
- x **Identify compliance challenges to achieve <2ppm**
- x **Distinguish the control efficiencies & operational parameters between SCR & CO catalysts**
- x **Describe excess emissions and causes of failure**



# NOx BACT Trends in CA

## Power Plant NOx BACT Trend: Combined-Cycle/Cogeneration Turbine Configurations

97% Reduction Since 1982



**BACT for power plants in 2000: 5 ppm**  
**BACT for power plants in 2005: 2.5 ppm**  
**BACT for power plants in 2012: 2 ppm**

# Future BACT Summary for Stationary Gas Turbines

	<b>NO<sub>x</sub></b>	<b>CO</b>	<b>VOC</b>	<b>PM<sub>10</sub></b>	<b>SO<sub>x</sub></b>
<b>Simple-Cycle &amp; Combined Cycle &amp; Cogen</b>	<b>1 - 2 ppm @ 15%O<sub>2</sub></b>  <b>&amp;</b>  <b>&lt; 2 - 5 ppm NH<sub>3</sub> slip</b>	<b>1 - 2 ppm</b>	<b>1 ppm</b>  <b>OR</b>  <b>0.0027 lbs/MMBtu (HHV)</b>	<b>Equiv. to natural gas with fuel sulfur &lt; 1 grain/100 scf.</b>  <b>Now NH<sub>3</sub> is constituent of PM<sub>2.5</sub></b>	<b>Equiv to natural gas with fuel sulfur &lt; 1 grain/100 scf (&lt; 0.55 ppmvd)</b>  <b>Now SO<sub>x</sub> is constituent of PM<sub>2.5</sub></b>



# Simple Cycle Power Plant



**10 Minutes Rapid startup 800 MW  
loading with a Tunable Diode  
Laser (TDL)  $\text{NH}_3$  CEMs**

# Compliance Challenges: <2ppm

- x Single point probes vs. multi point probes
- x Stratification ( $\text{NO}_x$ ,  $\text{NH}_3$  & CO)
- x Inlet & outlet  $\text{NO}_x$
- x Differential  $\text{NO}_x$  vs. calculated  $\text{NH}_3$
- x Ammonia slip challenge
- x Suspect cal gases
- x Instrument air for  $\text{O}_2$  cal
- x  $\text{NO}_x$  converter,  $\text{NH}_3$  scrubber
- x Moisture in sample line



**Stratification**



**Single Point Probes vs. Multi Point Probes**

**Case Study #1: Stratification on a LMS100 Power Plant**  
**16 point test on the stack. Results showing 26% stratification in**  
**NOx. 20.5% RATA : Overall Failure**

Port	Point	O2	CO2	NOx	CO
N	4	13.19	4.42	1.99	-0.42
N	3	13.19	4.42	1.93	-0.43
N	2	13.20	4.42	1.86	-0.43
N	1	13.20	4.42	1.86	-0.43
E	4	13.15	4.45	1.79	-0.43
E	3	13.15	4.46	1.68	-0.45
E	2	13.15	4.46	1.61	-0.44
E	1	13.17	4.45	1.64	-0.45
S	4	13.15	4.46	1.67	-0.44
S	3	13.15	4.47	1.62	-0.45
S	2	13.15	4.47	1.65	-0.46
S	1	13.27	4.40	1.71	-0.46
W	4	13.15	4.47	1.54	-0.47
W	3	13.16	4.47	1.61	-0.47
W	2	13.17	4.47	1.63	-0.48
W	1	13.17	4.47	1.63	-0.48
Average		13.17	4.45	1.71	-0.45
Max		13.27	4.47	1.99	-0.42
Min		13.15	4.40	1.54	-0.48
diff		0.12	0.07	0.45	0.06
Strat		0.9%	1.7%	26.3%	-12.7%



Port	Point	O2	CO2	NOx	CO
N	4	13.19	4.42	1.99	-0.42
N	3	13.19	4.42	1.93	-0.43
N	2	13.20	4.42	1.86	-0.43
N	1	13.20	4.42	1.86	-0.43
E	4	13.15	4.45	1.79	-0.43
E	3	13.15	4.46	1.68	-0.45
E	2	13.15	4.46	1.61	-0.44
E	1	13.17	4.45	1.64	-0.45
S	4	13.15	4.46	1.67	-0.44
S	3	13.15	4.47	1.62	-0.45
S	2	13.15	4.47	1.65	-0.46
S	1	13.27	4.40	1.71	-0.46
W	4	13.15	4.47	1.54	-0.47
W	3	13.16	4.47	1.61	-0.47
W	2	13.17	4.47	1.63	-0.48
W	1	13.17	4.47	1.63	-0.48
Average		13.17	4.45	1.71	-0.45
Max		13.27	4.47	1.99	-0.42
Min		13.15	4.40	1.54	-0.48
diff		0.12	0.07	0.45	0.06
Strat		0.9%	1.7%	26.3%	-12.7%

## RELATIVE ACCURACY AND BIAS CALCULATION

Test	Date	Start Time	End Time	RM NO <sub>x</sub> ppm	CEMS NO <sub>x</sub> ppm	Difference NO <sub>x</sub> ppm	Valid Run 1=yes, 0=no	% Diff.
1				2.590	1.800	0.790	1	30.5%
2				2.460	1.630	0.830	1	33.7%
3				2.450	1.560	0.890	1	36.3%
4				2.150	1.650	0.500	1	23.3%
5				1.400	0.820	0.580	1	41.4%
6				1.500	0.980	0.520	1	34.7%
7				1.550	1.100	0.450	1	29.0%
8				1.760	1.330	0.430	1	24.4%
9				2.230	1.690	0.540	1	24.2%
10							0	-
11							0	-
12							0	-
Average				2.010	1.396	0.614		30.8%

### Case Study #2: LM6000 April 2016

Emission Standard	2.5	ppm	
% of Standard	80.4%		
Ref. Method Average:	2.01	ppm	
Average Difference:	0.61	ppm	
Number of Tests:	9		
Standard Deviation:	0.17	ppm	
t Value:	2.306		
Confidence Coefficient:	0.13	ppm	
Relative Accuracy:	<b>37.23</b>	%	Reference Method
Allowable RA	<b>20</b>	%	Reference Method
Bias Adjustment Factor:	1.111		
Status	Fail		

## Case Study #2: LM6000 Gas Turbine

- x **NO<sub>x</sub> Compliance limit: 2.5 ppmvd @ 15% O<sub>2</sub>**
  - **Test result @ 2.5 ppmvd @ 15% O<sub>2</sub>: Pass**
- x **NO<sub>x</sub> Part 75 Relative Accuracy (RA): 10% or alternate criteria of ±0.02 lbs/MMBtu (RM vs CEM)**
  - **Test result of 37% RA (Fail) and 0.02 lbs/MMBtu (Pass)**
- x **NO<sub>x</sub> Part 60 Relative Accuracy (RA): 20% (No alternate criteria)**
  - **Test result of 37% RA (Fail)**
- x **NH<sub>3</sub> Compliance limit: 10 ppmvd @ 15% O<sub>2</sub>**
  - **Test result @ 8.2 ppmvd @ 15% O<sub>2</sub>: Pass**

## Single Point Probes vs. Multi Point Probes

- x **Stratification in plant will exist**
- x **SCR seals will fail & NH<sub>3</sub> distribution (AIG) change**
- x **SCR & CO configuration in plant changes**
- x **Test van traverses the stack in an “X” - Collects “Representative Sample”**
- x **CEMS probe likely to be a single point, may not match up on day of RATA**



# CO Catalyst Issues





**Improper Catalyst &  
Incorrect Catalyst  
Bed Temperature**

The image shows a large industrial facility, likely a power plant, with several tall, cylindrical smokestacks and a complex network of pipes and scaffolding. Red arrows point from text boxes to specific parts of the facility. One arrow points from the 'Improper Catalyst & Incorrect Catalyst Bed Temperature' box to a section of the piping. Another arrow points from the 'Catalyst Seal Fracture' box to a higher section of the same piping. A third arrow points from the 'Poor AIG Design Poor Air Mixing' box to a lower section of the piping. A fourth arrow points from the 'Insufficient NH<sub>3</sub> injection capability' box to a section of the piping. A fifth arrow points from the 'SCR & NO<sub>x</sub> Failure' box to a section of the piping. The background is a clear blue sky.

**Catalyst  
Seal  
Fracture**

**Poor AIG Design  
Poor Air Mixing**

**SCR & NO<sub>x</sub>  
Failure**

**Insufficient  
NH<sub>3</sub> injection  
capability**



## RELATIVE ACCURACY AND BIAS CALCULATION

Test	Date	Start Time	End Time	RM NO <sub>x</sub> ppm	CEMS NO <sub>x</sub> ppm	Difference NO <sub>x</sub> ppm	Valid Run 1=yes, 0=no	% Diff.
1				1.890	1.740	0.150	1	7.9%
2				1.640	1.700	-0.060	1	-3.7%
3				1.310	1.320	-0.010	1	-0.8%
4				1.420	1.590	-0.170	1	-12.0%
5				1.270	1.360	-0.090	1	-7.1%
6				1.500	1.500	0.000	1	0.0%
7				1.370	1.370	0.000	1	0.0%
8				1.450	1.440	0.010	1	0.7%
9				1.400	1.380	0.020	1	1.4%
10							0	-
11							0	-
12							0	-
Average				1.472	1.489	-0.017		-1.5%

Emission Standard      2.5      ppm  
 % of Standar      58.9%

Ref. Method Average:      1.47      ppm  
 Average Difference:      -0.02      ppm  
 Number of Tests:      9  
 Standard Deviation:      0.09      ppm  
 t Value:      2.306  
 Confidence Coefficient:      0.07      ppm

Relative Accuracy: **5.70**      %  
 Allowable RA      20      %

Bias Adjustment Factor:      1.000  
 Status      Pass

Reference Method  
 Reference Method

**Case Study  
 #2: LM6000  
 June 2016  
 (post fix)**

## RELATIVE ACCURACY AND BIAS CALCULATION

Test	Date	Start Time	End Time	RM NO <sub>x</sub> ppm	CEMS NO <sub>x</sub> ppm	Difference NO <sub>x</sub> ppm	Valid Run 1=yes, 0=no	% Diff.
1				1.250	1.480	-0.230	1	-18.4%
2				1.230	1.470	-0.240	1	-19.5%
3				1.490	1.770	-0.280	1	-18.8%
4				1.210	1.510	-0.300	1	-24.8%
5				1.240	1.480	-0.240	1	-19.4%
6				1.220	1.470	-0.250	1	-20.5%
7				1.260	1.610	-0.350	1	-27.8%
8				1.220	1.500	-0.280	1	-23.0%
9				1.220	1.470	-0.250	1	-20.5%
10							0	-
11							0	-
12							0	-
Average				1.260	1.529	-0.269		-21.4%

Emission Standard      2.5      ppm  
 % of Standard      50.4%

Ref. Method Average:      1.26      ppm  
 Average Difference:      -0.27      ppm  
 Number of Tests:      9  
 Standard Deviation:      0.04      ppm  
 t Value:      2.306  
 Confidence Coefficient:      0.03      ppm

Relative Accuracy: **23.67**      %

Allowable RA      20      %

Bias Adjustment Factor:      1.000

Status      Fail

Reference Method  
 Reference Method

**Case Study  
 #3: GE 7FA  
 175 MW  
 Turbine**



## Case Study #2: LM6000 Gas Turbine

- x **NO<sub>x</sub> Compliance limit: 2.5 ppmvd @ 15% O<sub>2</sub>**
  - **Test result @ 2.5 ppmvd @ 15% O<sub>2</sub>: Pass**
- x **NO<sub>x</sub> Part 75 Relative Accuracy (RA): 10% or alternate criteria of ±0.02 lbs/MMBtu (RM vs CEM)**
  - **Test result of 24% RA (Fail) and 0.02 lbs/MMBtu (Pass)**
- x **NO<sub>x</sub> Part 60 Relative Accuracy (RA): 20% (No alternate criteria)**
  - **Test result of 24% RA (Fail)**
- x **NH<sub>3</sub> Compliance limit: 10 ppmvd @ 15% O<sub>2</sub>**
  - **Test result @ 5.5 ppmvd @ 15% O<sub>2</sub>: Pass**

# Gas Turbine Inlet & Outlet NO<sub>x</sub>



## Gas Turbine Inlet & Outlet NOx

- x **Outlet NOx is mandatory**
- x **Inlet NOx maybe optional**
- x **Measuring both will represent better identify compliance target**
- x **Is NH<sub>3</sub> slip a mathematical calculation using a bias #?**
- x **Differential NOx vs. calculated NH<sub>3</sub> slip**



# NH<sub>3</sub> Slip Bias Calculation

Unit 1 - Max				
Ammonia Slip				
NH <sub>3</sub> Test No.	1-NH3-MAX-1	2-NH3-MAX-1	3-NH3-MAX-1	Averages
Date	2/27/15	2/27/15	2/27/15	--
Time	1701-1750	1817-1847	1854-1924	--
Process Data:				
NH <sub>3</sub> Solution Injection Rate, lb/hr	260.99	256.22	259.10	258.77
lb NH <sub>3</sub> per lb of solution	0.28	0.28	0.28	0.28
Fuel Flow rate, MMBtu/hr	2,028.8	2,027.4	2,027.2	2,027.8
NH <sub>3</sub> injected, equivalent as ppm vol. dry	34.64	33.9	34.33	34.30
Gaseous Emissions (Inlet)				
NO <sub>x</sub> Inlet, ppm volume dry	32.4	31.8	32.3	32.2
Gaseous Emissions (Outlet)				
O <sub>2</sub> Outlet, % volume dry	13.18	13.20	13.21	13.19
NO <sub>x</sub> Outlet, ppm volume dry	2.48	2.56	2.62	2.55
Measured NH <sub>3</sub> Slip, ppm volume dry @ 15% O <sub>2</sub>	3.25	2.67	2.28	2.73
NH <sub>3</sub> Slip raw calc, ppm volume dry @ 15% O <sub>2</sub>	3.61	3.60	3.56	3.59
NH <sub>3</sub> Slip Correction Factor	0.90	0.74	0.64	0.76



Unit 1 - Max					
Ammonia Slip					
NH <sub>3</sub> Test No.		1-NH3-MAX-1	2-NH3-MAX-1	3-NH3-MAX-1	Averages
Date		2/27/15	2/27/15	2/27/15	--
Time		1701-1750	1817-1847	1854-1924	--
Process Data:					
NH <sub>3</sub> Solution Injection Rate, lb/hr		260.99	256.92	259.10	258.77
lb NH <sub>3</sub> per lb of solution		0.28	0.28	0.28	0.28
Fuel Flow rate, MMBtu/hr		2,028.8	2,027.4	2,027.2	2,027.8
NH <sub>3</sub> injected, equivlent as ppm vol. dry		34.64	33.94	34.33	34.30
Gaseous Emissions (Inlet)					
NO <sub>x</sub> Inlet, ppm volume dry		32.4	31.8	32.3	32.2
Gaseous Emissions (Outlet)					
O <sub>2</sub> Outlet, % volume dry		13.18	13.20	13.20	13.19
NO <sub>x</sub> Outlet, ppm volume dry		2.48	2.56	2.62	2.55
Measured NH <sub>3</sub> Slip, ppm volume dry @ 15% O <sub>2</sub>		3.25	2.67	2.28	2.73
NH <sub>3</sub> Slip raw calc, ppm volume dry @ 15% O <sub>2</sub>		3.61	3.60	3.56	3.59
NH <sub>3</sub> Slip Correction Factor		0.90	0.74	0.64	0.76

# **NH<sub>3</sub> Injection Grid (AIG)**



# New Permits for Anhydrous $\text{NH}_3$ Maybe be Challenging







**NH<sub>3</sub> Injection Vaporizer Skid**





**NH<sub>3</sub> Vaporizer Skid: Redundant Backup Electric Heaters**

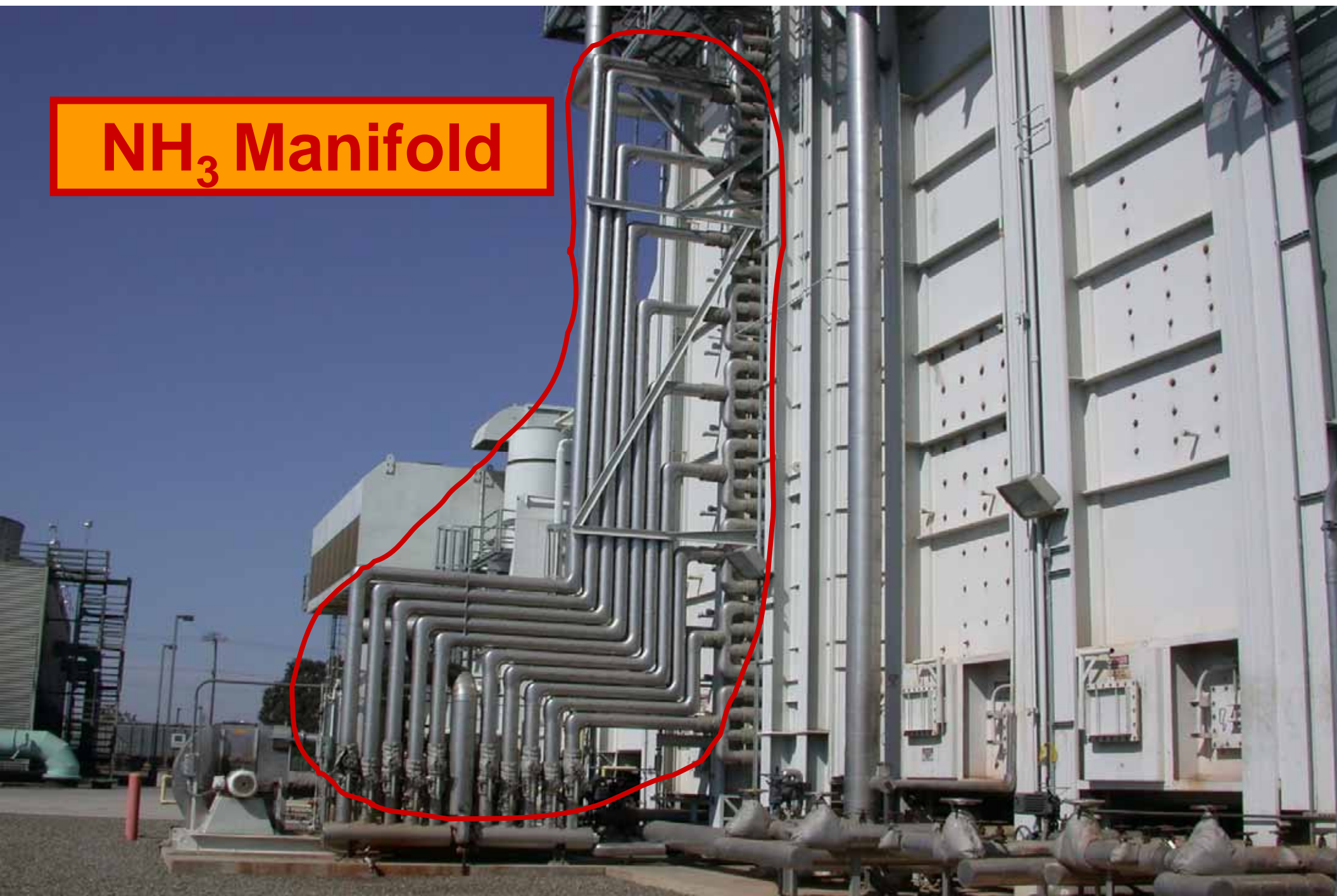


**NH<sub>3</sub> Lines**

↑ **AMMONIA** ↑



**NH<sub>3</sub> Manifold**







**NH<sub>3</sub> Lines**

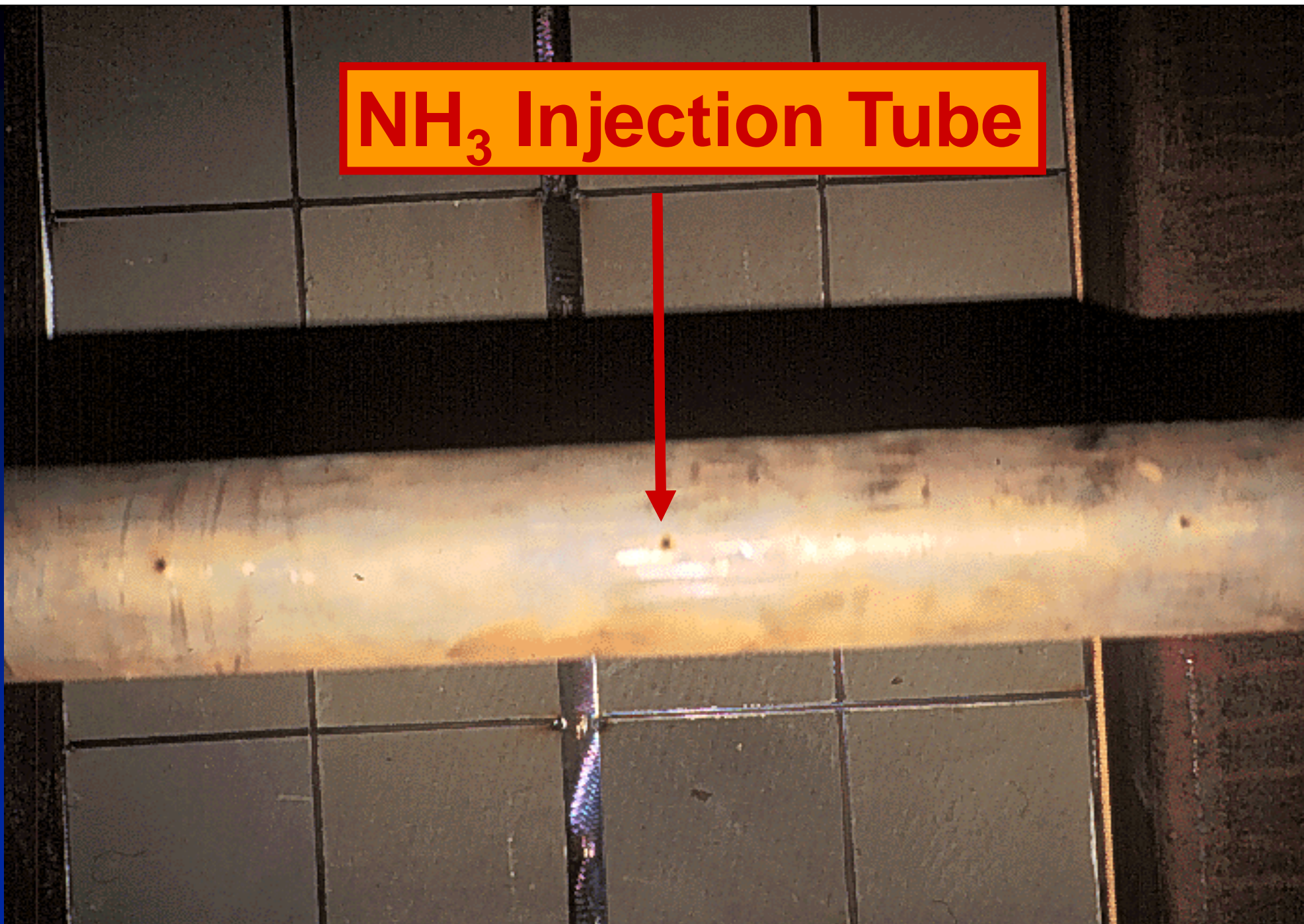
A photograph of a large industrial facility, likely a power plant or refinery, featuring a complex network of metal pipes, structural steel, and scaffolding. A red arrow points from the 'NH<sub>3</sub> Lines' label to a specific set of pipes. Another red arrow points from the 'HRSG' label to a large cylindrical structure on the right. A third red arrow points from the 'Cost of NH<sub>3</sub> Slip' label to a lower section of the piping.

**HRSG**

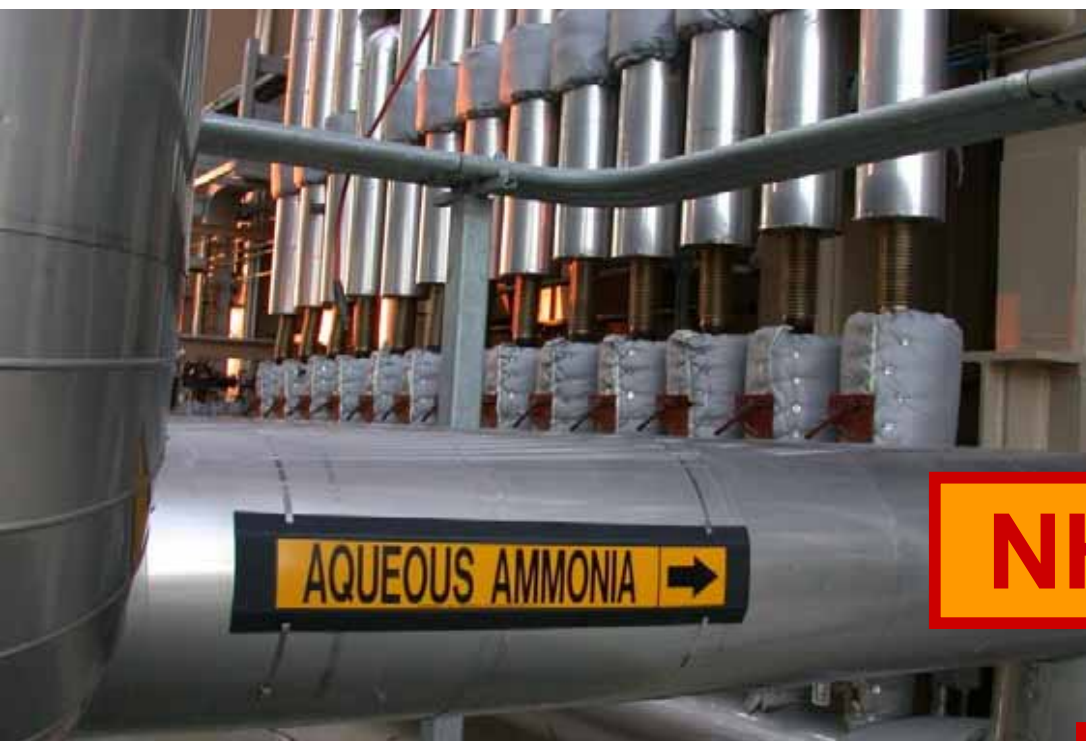
**Cost of NH<sub>3</sub> Slip (EPA)**  
— 1 ppmv of NH<sub>3</sub> Slip =  
\$35,000/year



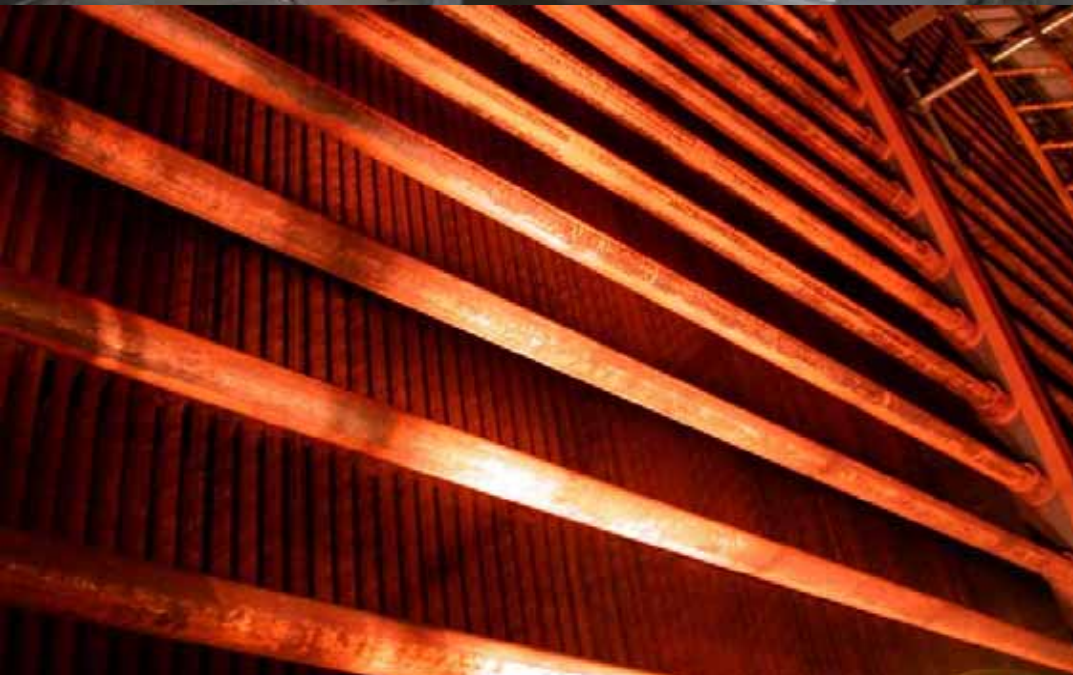
**NH<sub>3</sub> Injection Tube**







**$\text{NH}_3$**



- **Issues With  $\text{NH}_3$** 
  - Even Distribution
  - Proper Mixing Temp.
  - Fast start-up
  - Thermal Expansion
  - Balancing manifold
  - Access & maintenance



**What Constitutes  
Excess Emission  
Events (>2ppm  
NO<sub>x</sub>) and  
Breakdown?**

## **Excess Emission Events (>2 ppm NOx) and Breakdown**

- x CEM analyzer and sample train failure**
- x Ammonia deposits due to poor water quality from the ammonia supply vendor (nozzle plugging)**
- x Ammonia electric heater failure (degradation in the spray nozzle and / or deflector plate leading to poor vaporization)**
- x Ammonia pump failure**

## **Excess Emission Events (>2 ppm NOx) and Breakdown**

- x Ammonia dilution blower failure**
- x Ammonia hot exhaust blower failure**
- x 650F exhaust, 5' blower fan radius @ 3600 rpm**
- x SCR heater controller cabinet overheats because it's getting baked in the sun**
- x On hot days, when anhydrous NH<sub>3</sub> tank is low, it is possible for pumps to vapor lock, shutting down NH<sub>3</sub> injection**

## **Excess Emission Events and Breakdown**

- x NOx water injection pump & valve failure**
- x Engine vibrations & harmonics lead to trips**
- x Emissions spikes (due to load change) after CEMS are put back into service after maintenance or calibration**
- x Turbine bearing and blade failures**
- x Retrofit from peaker to combined cycle but keep same SCR...now ask for a variance!!**



## **Excess Emission Events and Breakdown**

**Extremely low emission limits and/or short averaging periods lead to events.**

**Any small hiccups to the turbine, control system, or monitoring system can lead to small emission spikes that can make it impossible to meet limits.**

## **Excess Emission Events and Breakdown**

**It is increasingly important that permits be configured to allow for these type of events**

***(X number of allowable excursions, Y number of Start-ups and Shut-downs per hour and per day, Z number of allowable lbs of NOx per hour and day etc.)***



## **RATA Tips & Points of Failure**

## **RATA Tips & Points of Failure**

- x Peaking plants don't run all the time – run it the week / day before the test to check things out**
- x Perform preventative maintenance on the analyzers and CEMS system before RATA**
- x Check the Water Knockout – draining ?**
- x Check the ammonia scrubber system – looks good? Change out media?**
- x Check the NOx analyzer – is the NO<sub>2</sub> converter working?**

## **RATA Tips & Points of Failure**

- x Check the PLC & DAS for accuracy**
- x Check heated lines**
  - Do they have a downward slope throughout the line?**
  - No cold spots?**
  - Are they warm to the touch?**
- x The Test Van is CORRECT (the EPA Reference Method). PGVP gases with a good Zero gas.**



## **RATA Tips & Points of Failure**

- x Stack Platform – Take a look inside: CEMS probe look good? Is it there?**
- x Stack Platform – Are platforms / railings safe and sound? Loosen bolts on sample ports (be nice to your tester)**
- x Stack Platform – Do all of the connections and valves look good?**

## **RATA Tips & Points of Failure**

- x Balance the NO<sub>x</sub> and the Ammonia slip – so that you pass both at the same time.**
- x Check for SCR seal leaks and stack stratification. Good idea to install multi-point probes in the stack.**
- x It is good to run with the highest allowed NO<sub>x</sub> emissions**
  - It will make the RATA equation easier to pass, and**
  - you will have the lowest ammonia emissions.**

## **RATA Tips & Points of Failure**

- x Do a Linearity or Cylinder Gas Audit before RATA day**
- x Perform Site CEMS calibration early – complete well before the RATA test. Do a manual calibration as well. Swap bottles with tester for accuracy.**
- x An extra check that everything is good will make compliance easier**



**Questions ?**